

High-power CW Transmission Systems and Launchers

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- Introduction: CW / long-pulse transmission systems for ECRH
- HE11 corrugated waveguide transmission
- Beam waveguide transmission
- Matching problems
- Diagnostic components: CW power monitors and CW loads
- Launchers and in-vessel components: W7-X, ITER, Tore Supra
- Summary

Thanks to

G. Denisov and V. Malygin, IAP N. Novgorod

J. Lohr, GA San Diego

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G. Dammertz, FZK Karlsruhe

H. Laqua, F. Leuterer, H. Hollmann, M. Weißgerber, IPP Garching/Greifswald

K. Sakamoto and K. Takahashi, JAERI, Mito

R. Magne and M. Lennholm, CEA Cadarache

Some present and future long-pulse / CW ECRH / ECCD Systems:

DIII-D	110 GHz	6 gyrotrons		3.5 MW / 3 sec	in plasma
JT-60	110 GHz	4 gyrotrons		3 MW / 3 sec	in plasma
Tore Supra	118 GHz	> 2 gyrotrons		0.71 MW / 25 sec	in plasma
LHD	84 / 168 GHz	7 pulsed + 1 CW gyrotron		0.072 / 766 sec	in plasma
W7-X	140 GHz	10 gyrotrons	design:	10 MW CW inst.,	in construction
ITER	170 GHz	24 gyrotrons	design:	24 MW CW inst.,	in development

- Typical goals are 1 MW / 10 sec CW per line
- Developments for ITER aim at 2 MW CW per line

==> **corrugated waveguides** (HE11 mode)

==> **(multi)-beam waveguides** (TEM00 mode)

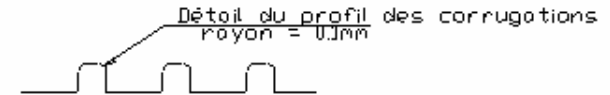
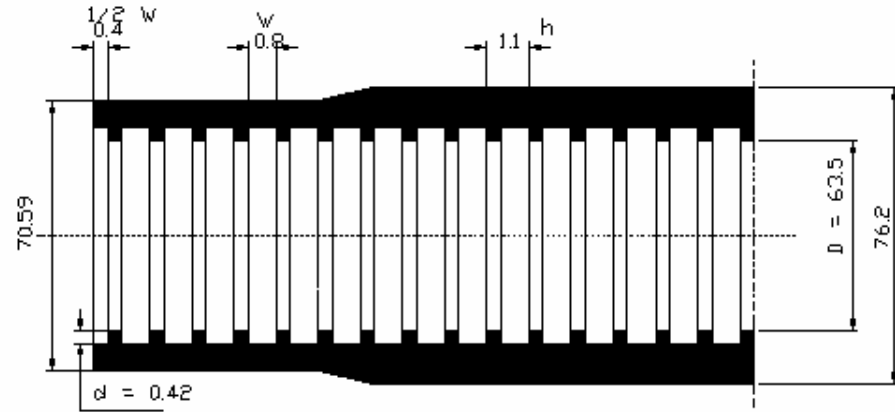
==> **launchers with toroidal and poloidal steering**

**For high efficiency
and high reliability:
low loss !**

Corrugated waveguide transmission

Propagation of HE₁₁ mode

$$E(r, z) \propto J_0\left(\frac{2.405 \cdot r}{a}\right) \cdot e^{ik_{11}z}$$



waveguide loss for HE₁₁:

loss increases with mode number

==> low loss

==> high-order-mode filtering

curvature / tilt of waveguide

==> mode conversion loss (low-order modes)

mitre bends

==> mode conv. Loss (mainly high-order modes)

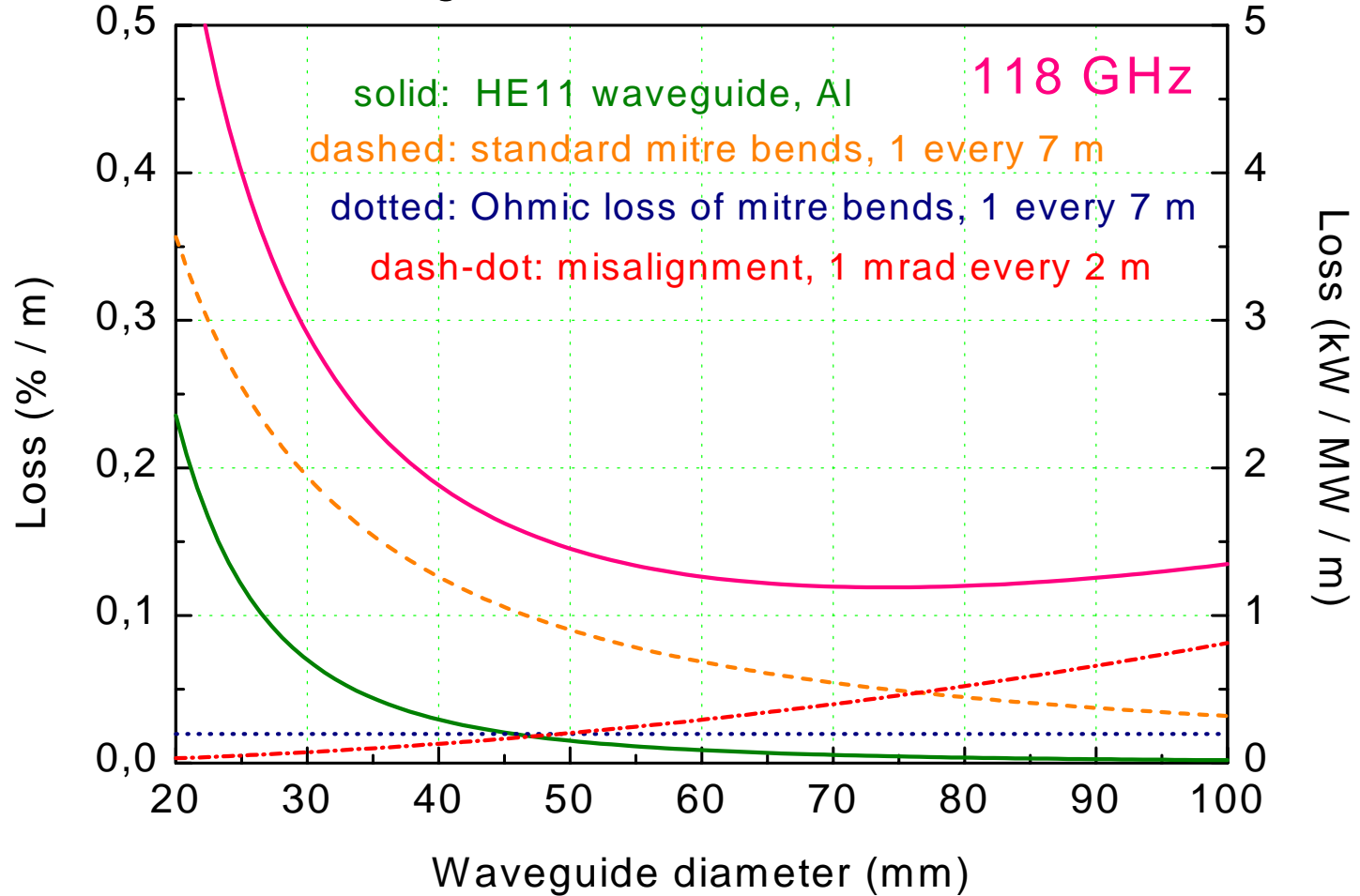
==> ohmic loss

Transmission in air:

==> atmospheric absorption

(H₂O, O₂ around 60, 118 and 180 GHz)

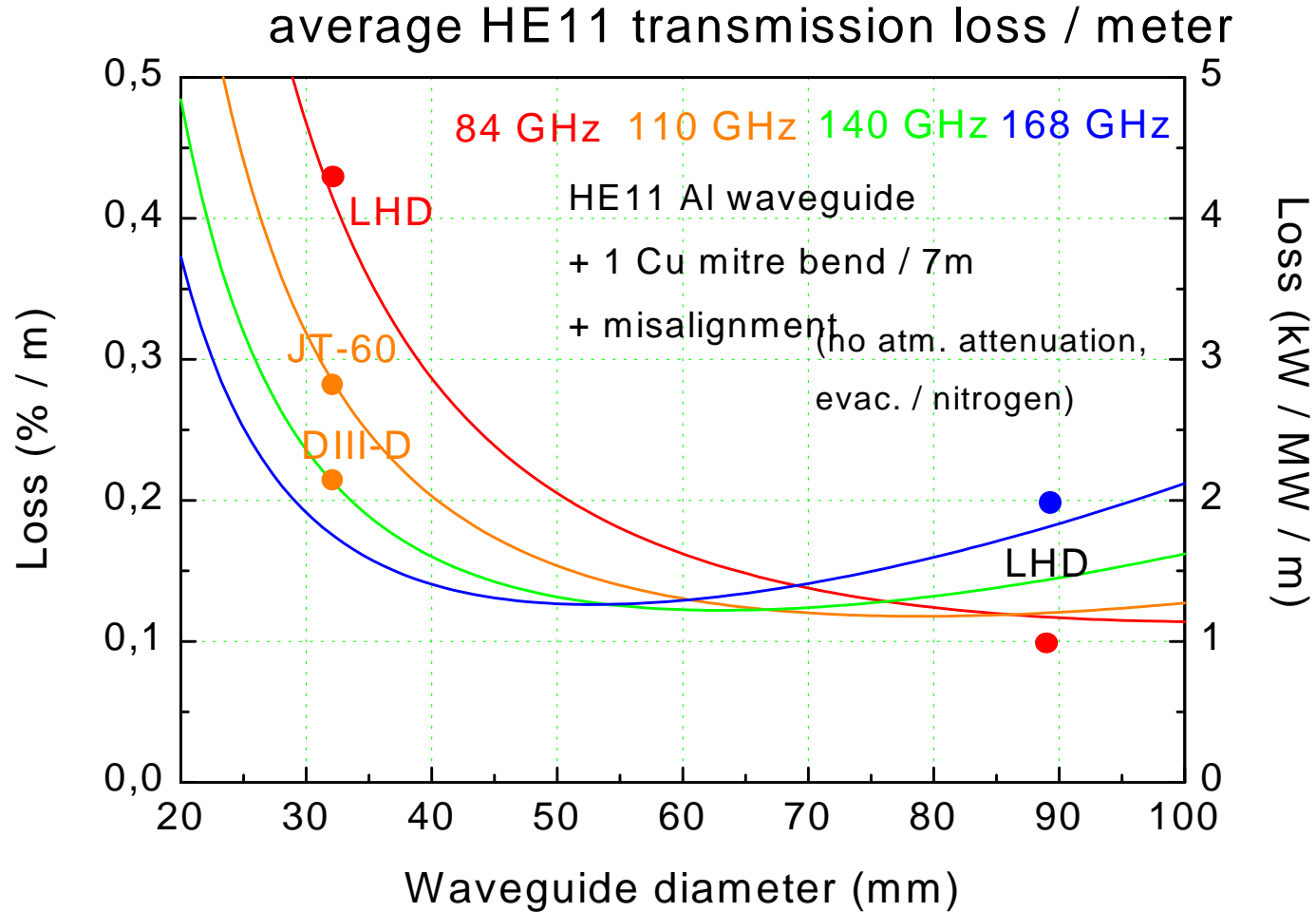
average HE11 transmission loss / meter



Small diameter (low frequencies): Mitre bends and waveguides produce most of loss

Large diameter (high frequencies): High-precision components + careful alignment required

Optimization of waveguide diameter



Results of transmission lines agree well with theory (examples > 60 m)

For ITER, $D = 63.5$ mm gives nearly minimum loss and is compatible with 2 MW

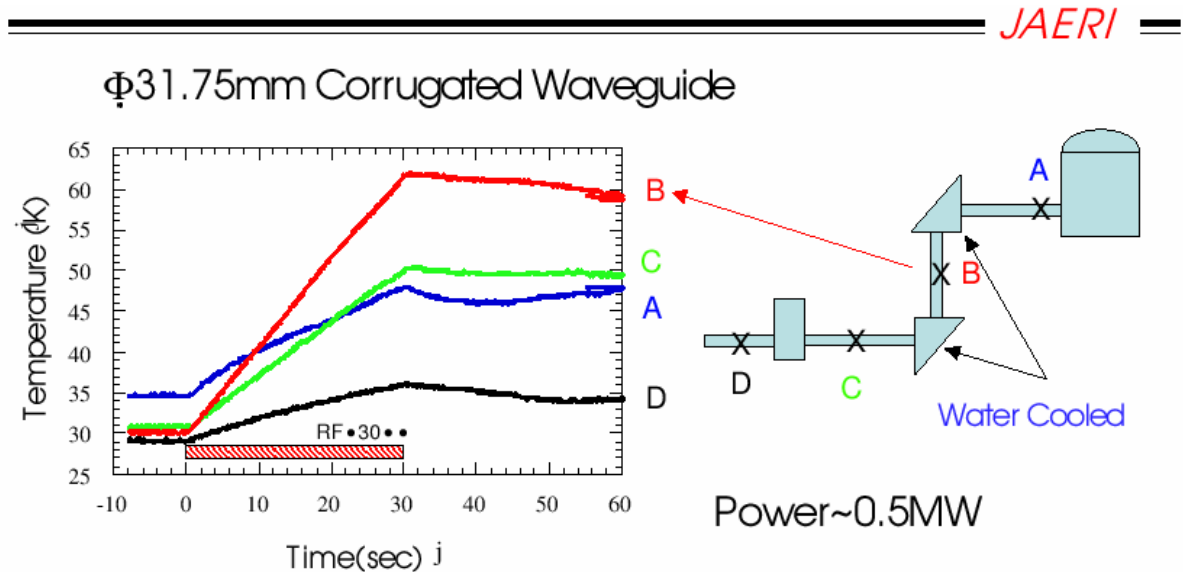
Mitre bends excite higher-order modes due to internal diffraction

==> **main source of arcing** in non-evacuated waveguides

==> high-order modes are **subsequently damped in waveguide**

==> **waveguide must be cooled for CW-operation!**

Experiment at JAERI:



==> **use diffraction-reduced bends!** ==> Improvement 2.....8

Phase corrected mirrors

Rippled wall HE11-HE12 partial mode converters (Doane and Moeller, 1994)

Mode-converting horn-mode type bends (IAP Nizhny Novgorod)

+ mode-filtering gaps + larger diameter +..... **Can water-cooling of waveguide be avoided?**



IAP



GYCOM

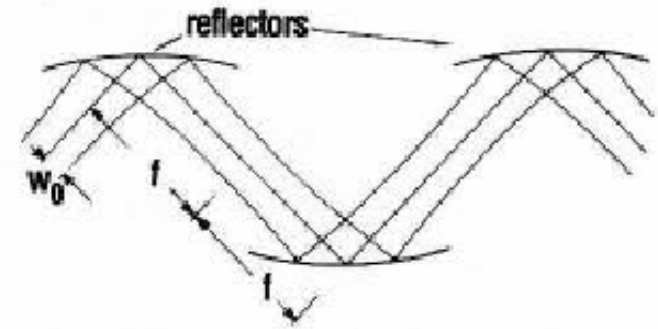
Test of the transmission line 82.7GHz /200kW /CW



$$P_0 = 200 \text{ kW} , \quad \tau = 1000 \text{ sec.} , \quad \eta_{\text{tr.line}} = 95\%$$

Beam transmission

Propagation of gaussian beam
by iterative focussing with reflectors



$$E(x, y, z) \propto e^{-\frac{x^2 + y^2}{w(z)^2}} \cdot e^{-ik \frac{x^2 + y^2}{2R(z)}} \cdot e^{i\Theta(z)}$$

For higher order modes m,n:

diffraction increases with mode number

Phase factor $\theta_{mn}(z) = (1+m+n) \theta(z)$

==> mode filtering

==> imaging properties

Curved mirrors lead to beam distortion

==> mode conv. Loss

Imperfect mirror surface, truncation

==> diffraction loss

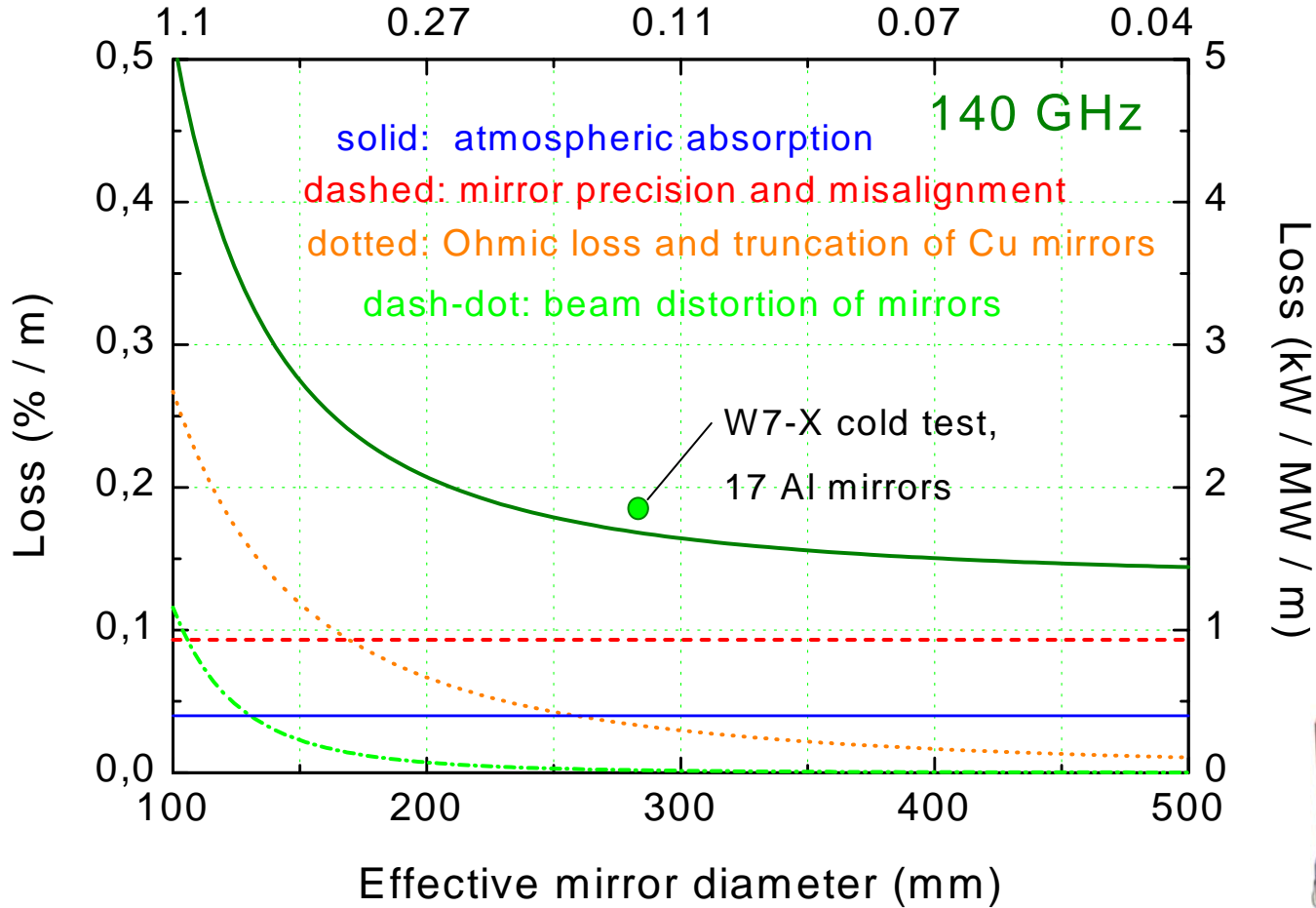
Transmission in air:

==> atmospheric absorption

(H₂O, O₂ around 60, 118 and 183 GHz)

Typical beam waveguide loss / meter

average number of mirrors / meter



Loss (kW / MW / m)

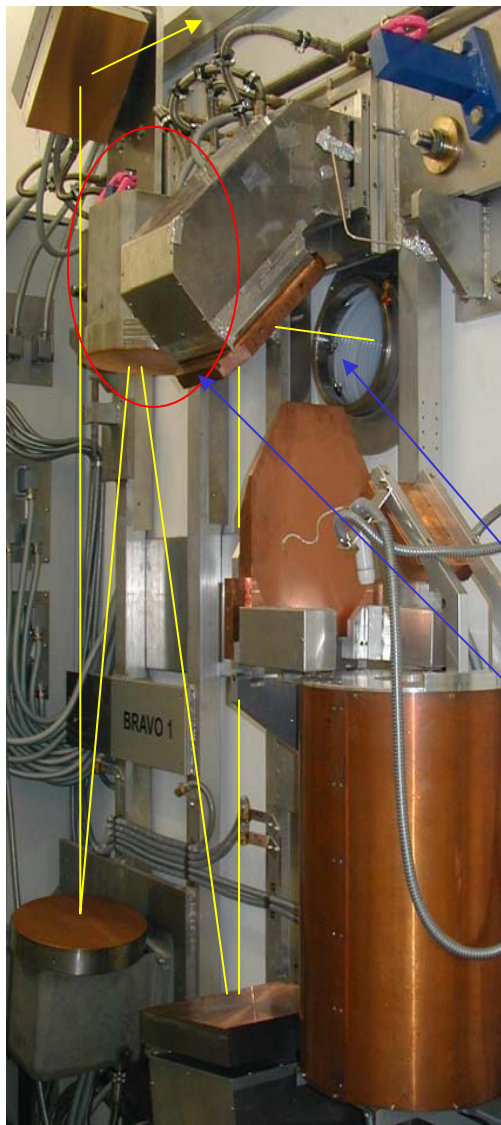


==> Beam diameter must be sufficiently large

==> High-quality components and alignment is essential

==> Air cooling, (+ drying or flushing with nitrogen) and stray radiation absorbers

W7-X optical transmission: Cooled components and installations



air cooling 200 kW

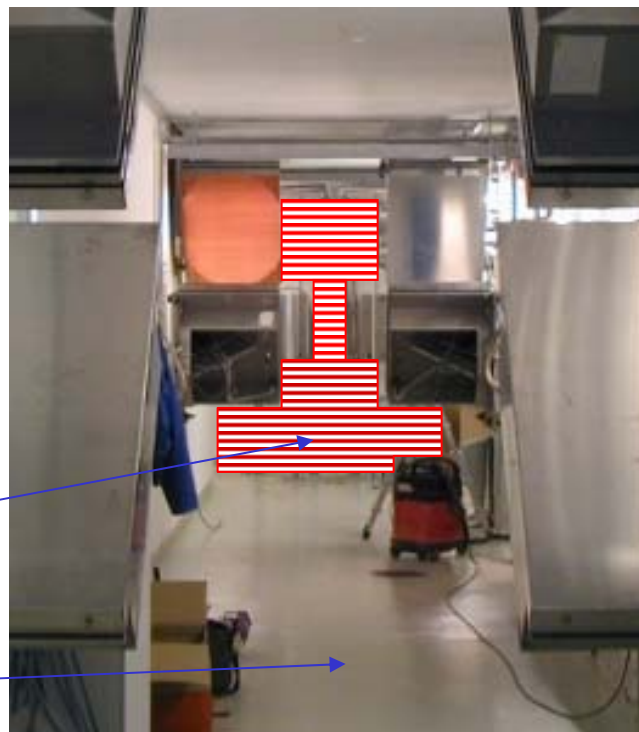
mirror cooling, ≤ 300 kW

**absorbing tube (Teflon hoses)
for gyrotron beam ≤ 300 kW**

**M1 stray radiation absorber
(not installed), ≤ 200 kW**

**Actively cooled stray radiation
absorbers, ≤ 300 kW**

**concret walls / floor to absorb
remaining radiation, ≤ 200 kW**



The W7-X Gyrotron test stand at FZK:

Test of mirrors, dummy load and rf-diagnostics with powers up to 890 kW / 180 sec



**140 GHz
gyrotron**

Matching optics M1, M2:
no visible problems

Polarizers (sinusoidal corrugation):
no arcing, if polarizers are clean
==> increase of power capability
of the dummy load)

directional coupler
using an integrated waveguide
==> CW-compatible

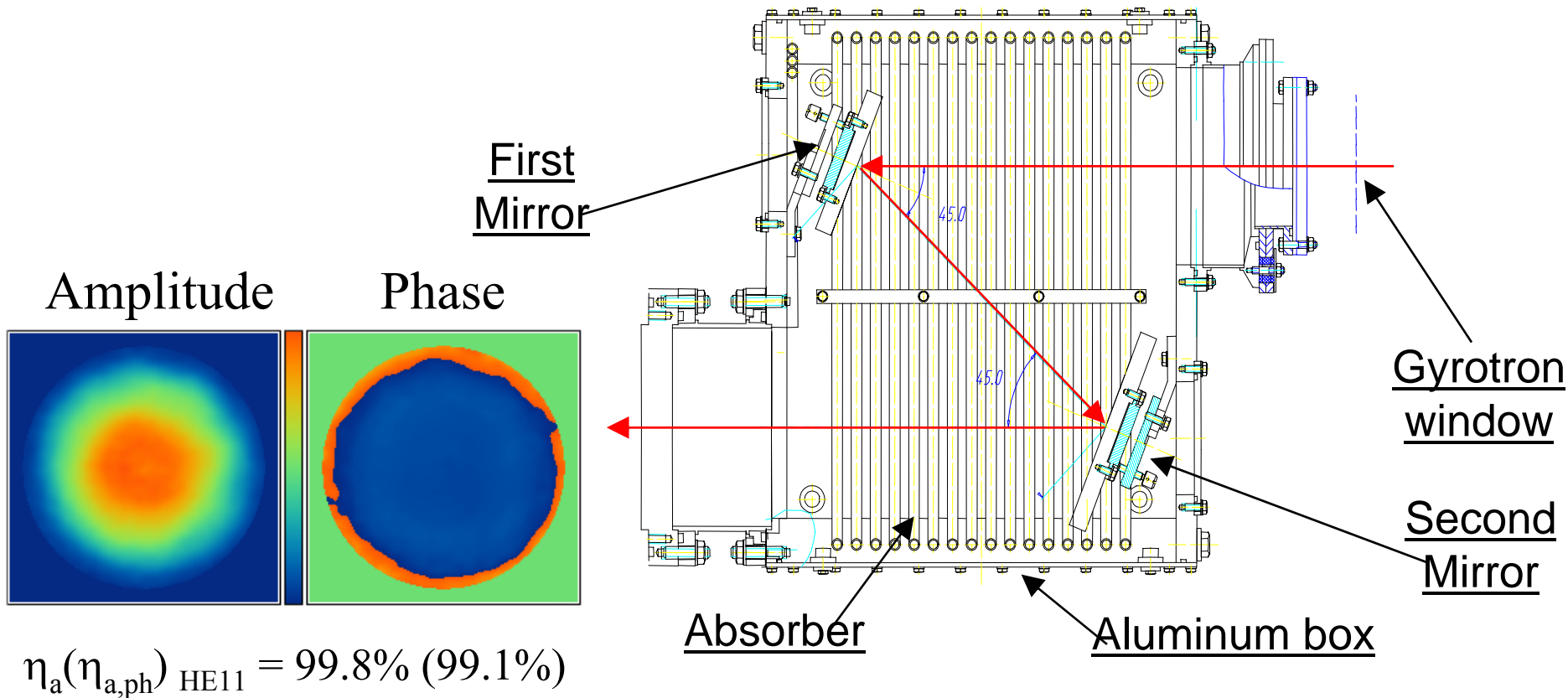
Matching of the gyrotron beam to the transmission line

Efficient methods available to transform gyrotron beam to HE11 or TEM00

Typical set-up: 2 phase-correcting mirrors



Institute of Applied Physics Academy of Sciences



High quality of output beams reached, but:

- **High alignment accuracy needed:** for HE_{11} : \implies mode conversion
for TEM_{00} : \implies misaligned gaussian beam
- **Alignment usually done with short pulse**
 - \implies Long-term mechanical stability of internal mirrors and MOU mirrors
 - \implies Frequency stability of gyrotron \implies varying output of beam ≤ 500 ms, $d/w_0=0.25$
- **Stray radiation from inside the gyrotron is not re-converted**
 - \implies risk of enhanced reflection back to the gyrotron

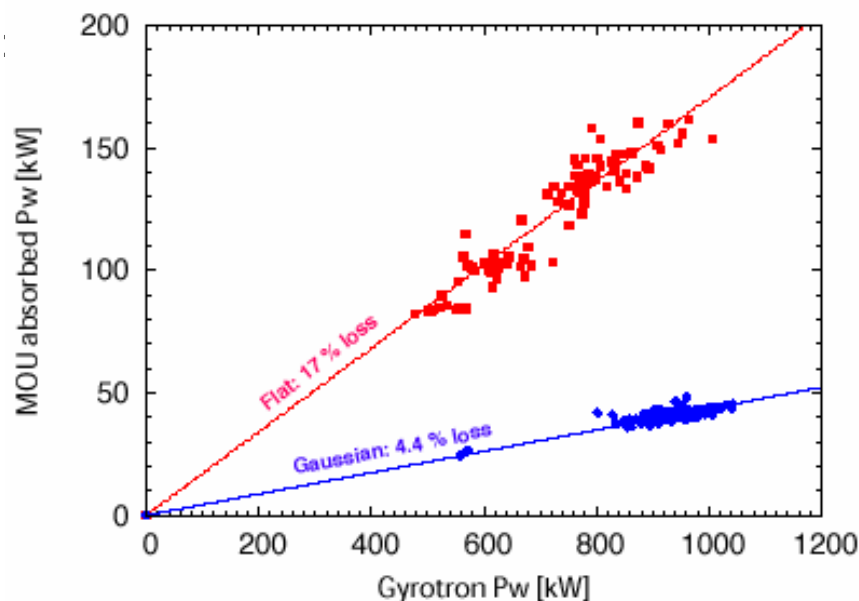
J. Lohr et al, GA San Diego:
comparison of MOU loss

gyrotrons with

ext. Phase correction

gaussian beam,

(single mirror MOU)



WANTED for CW:

Gyrotrons with

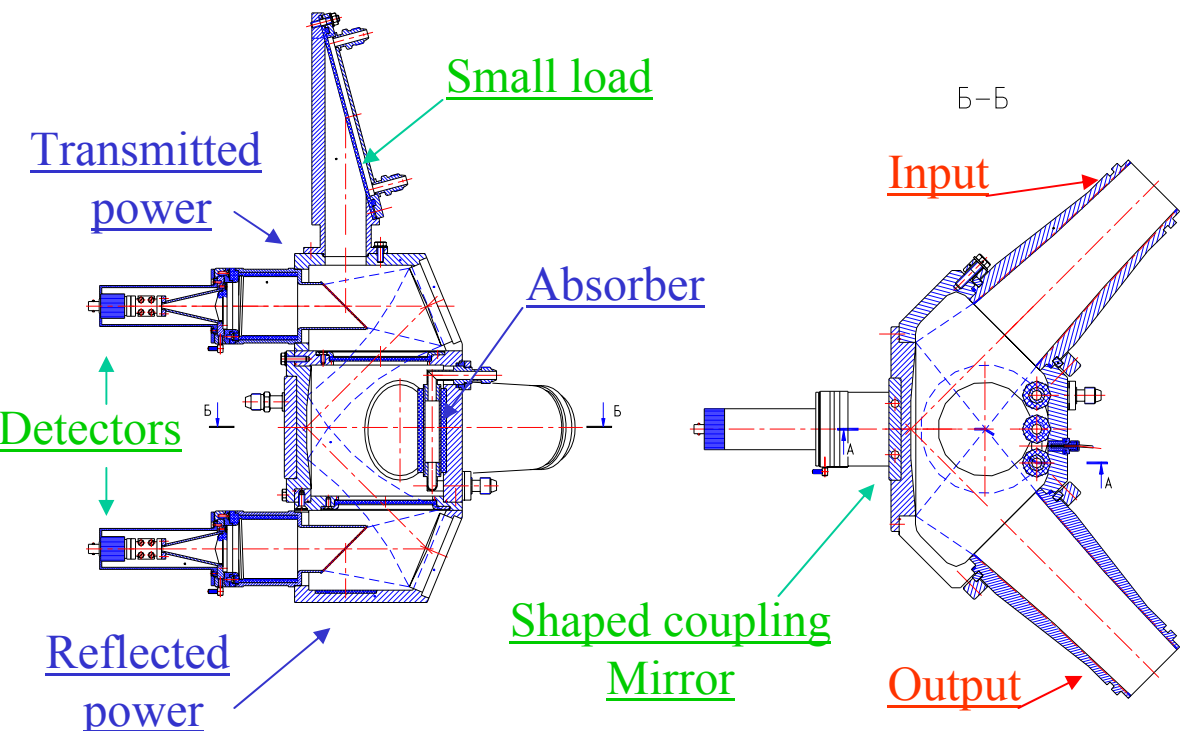
high beam quality and

low stray radiation



Meter of transmitted and reflected power in a quasi-optical miter bend

Grating coupler:

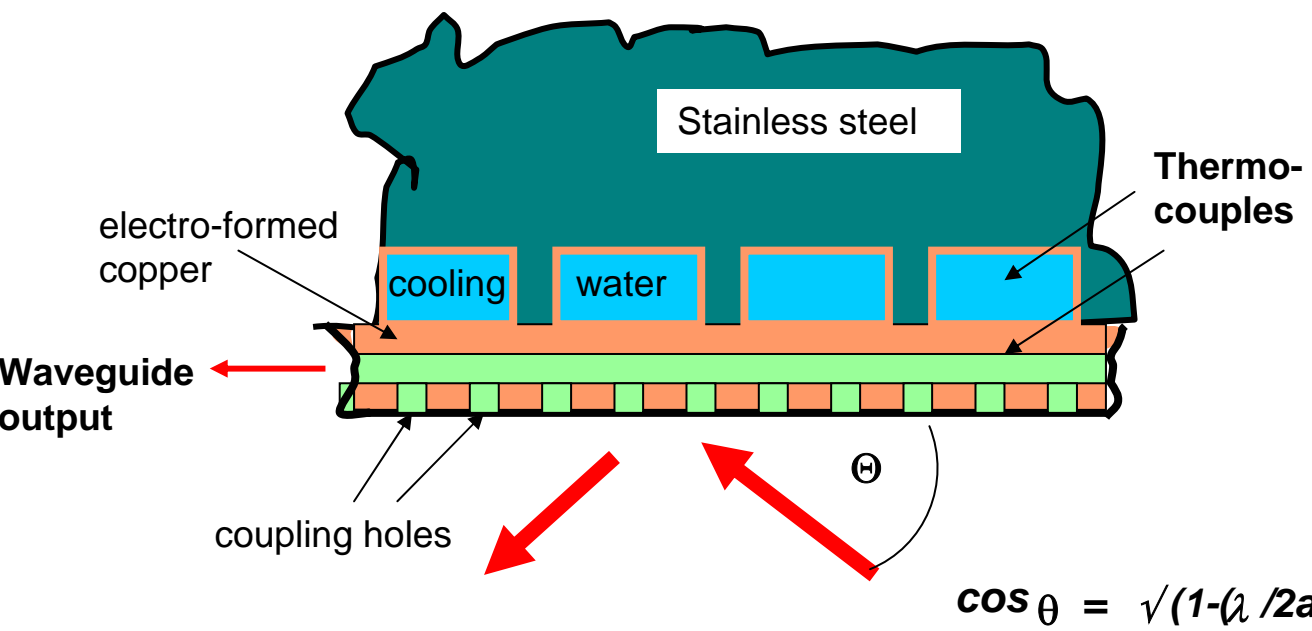


Measuring channels

Main channel

Diffraction losses – 0.1%

Compact power monitors for water-cooled (mitre bend) mirrors

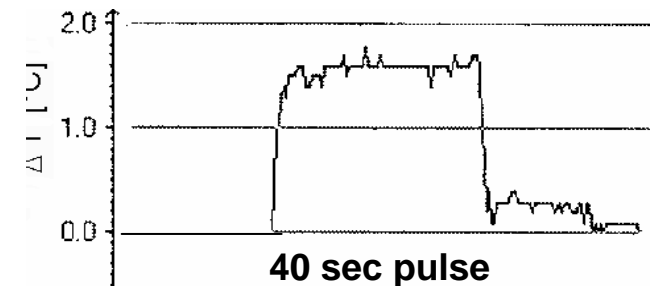
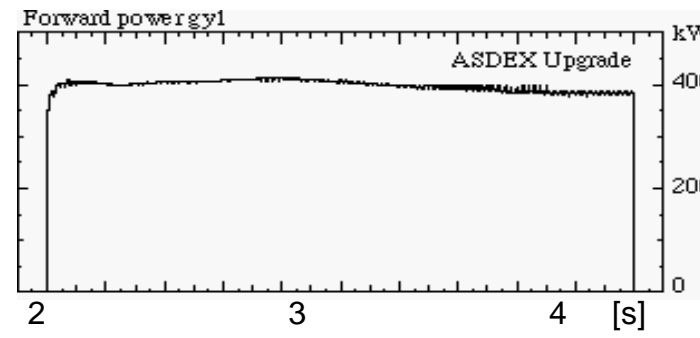


waveguide coupler:

coupling of radiation to monomode waveguide,
RF measurement

Thermocouples:

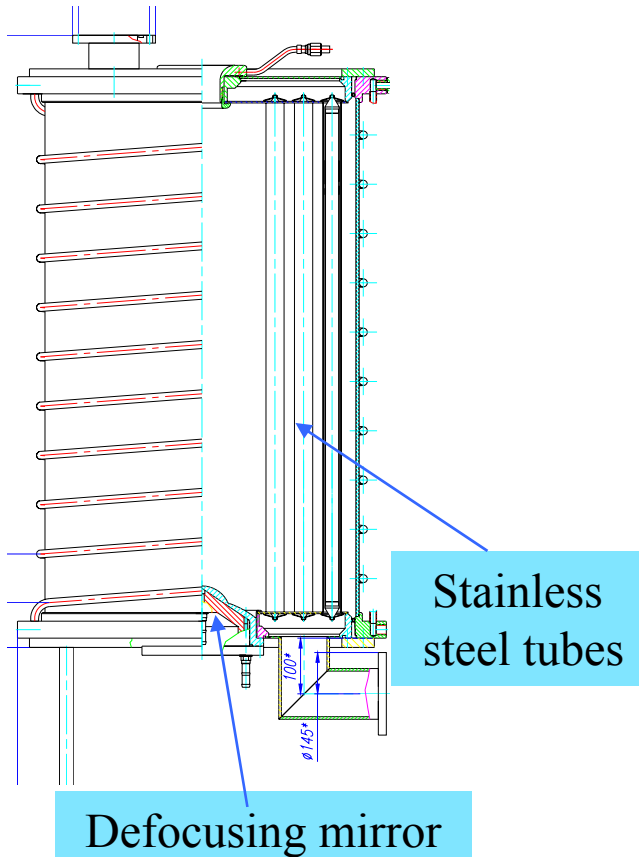
calorimetric power measurement: $P \propto T(\text{outlet}) - T(\text{inlet})$,
 $P \propto T(\text{copper}) - T(\text{water})$



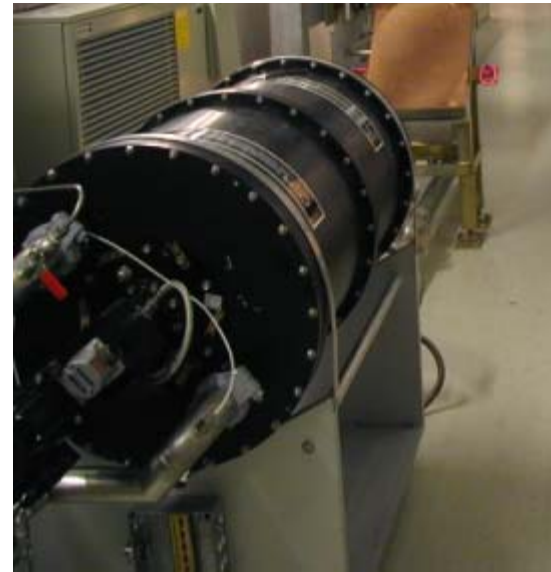
Calorimetric loads, designed for 1 MW CW:



IAP N. Novgorod:



- Typical problems:
- reflection of a few percent
 - quality of coating (CCR)

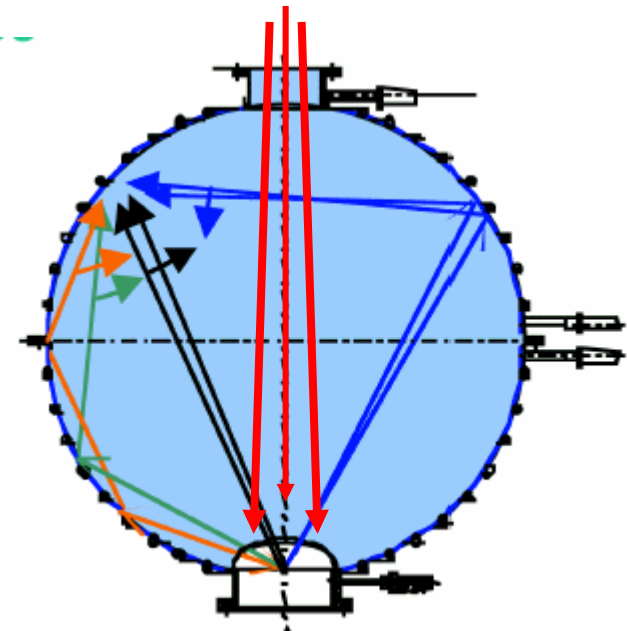


Calabazas
Creek
Research:

rotating mirror
TiO₂ -absorber

IFP Milano:

spherical load
CrO₂ - absorber

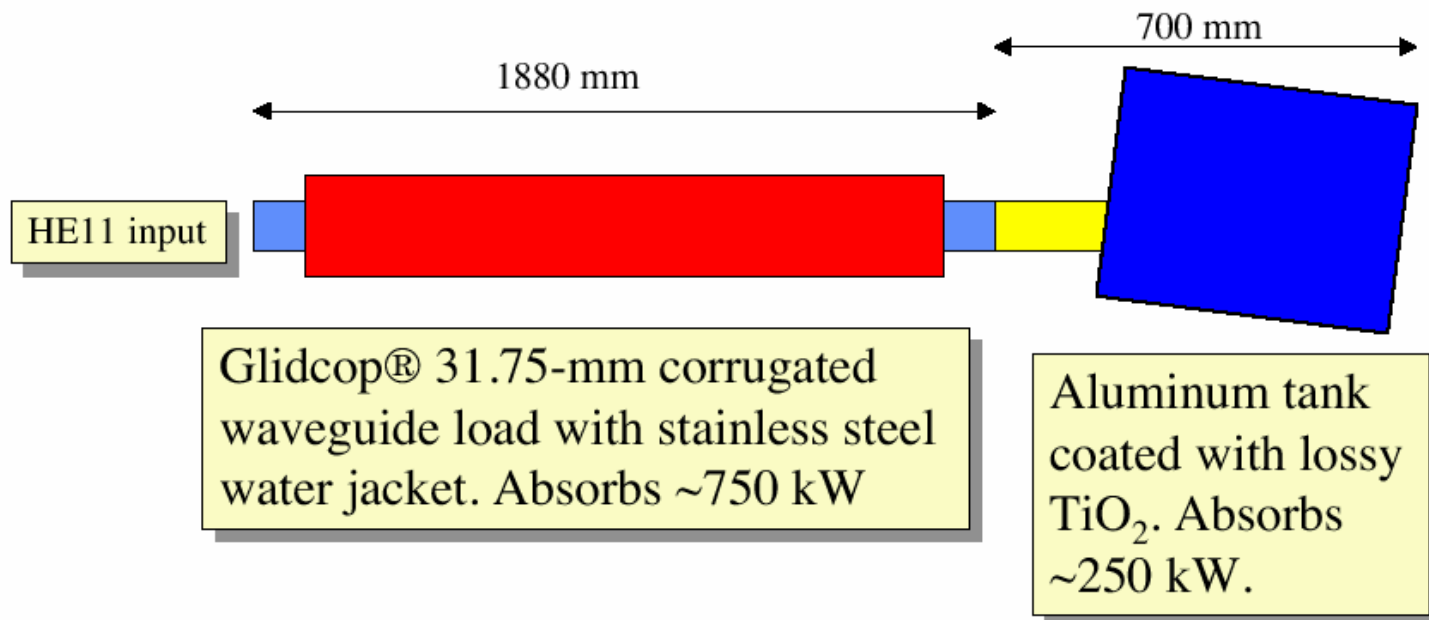


==> Loads must often be used with a pre-load

==> Alternative solution: waveguide with strong attenuation followed by load



Schematic of 1-MW CW load



Launchers for CW ECRH / ECCD

Requirements

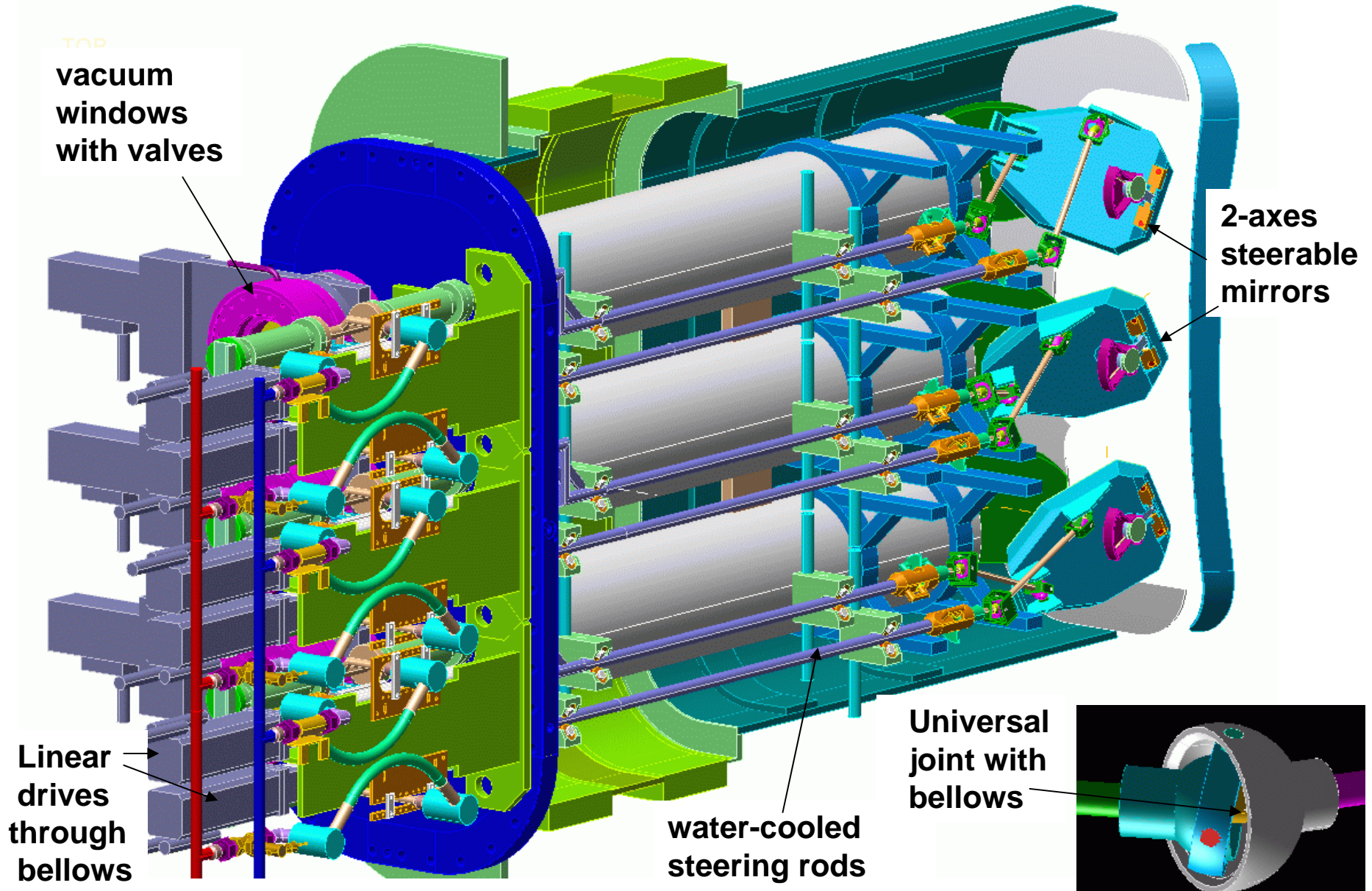
- poloidal and toroidal beam steering
- fast steering to follow NTMs
- high reliability

Examples:

- fast movable launchers on DIII-D, JT-60 and ASDEX-Ug,
ITER Upper Launcher ==> talks this conference
- W7-X plug-in launchers
- ITER mid-plane launcher
- Tore Supra

W7-X plug-in launcher:

4 launchers with 3 individual antennas each



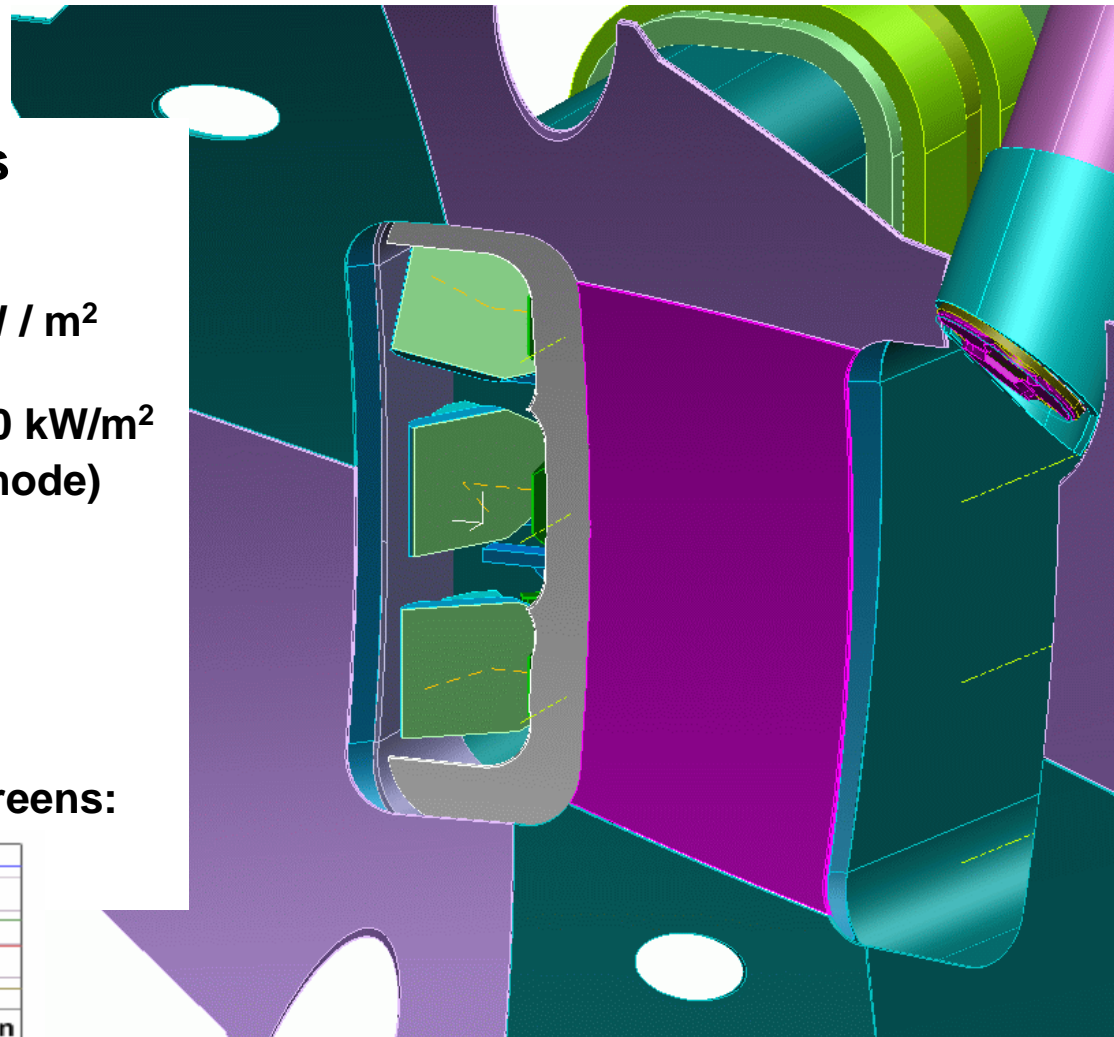
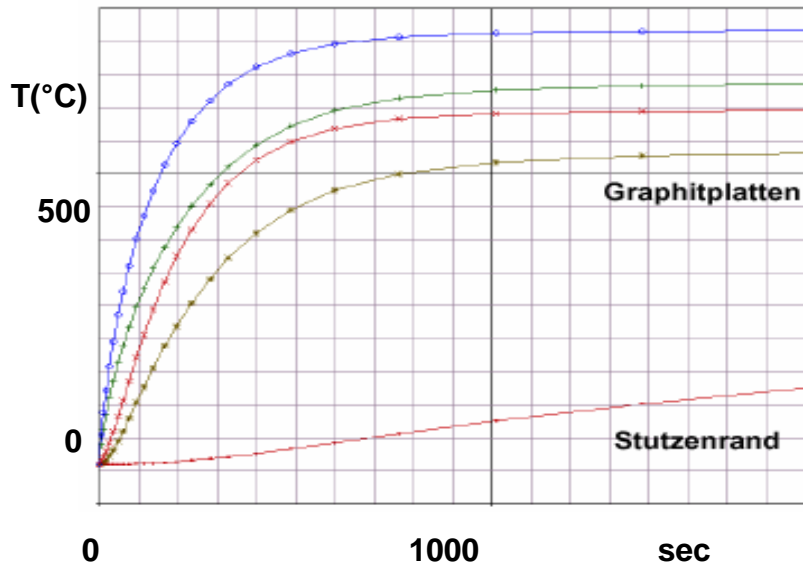
Heat loads in W7-X launchers

Plasma radiation: $< 100 \text{ kW / m}^2$

Diffuse mm-wave radiation: $10 \dots 200 \text{ kW/m}^2$
(low for X2-mode, high for O2-mode)

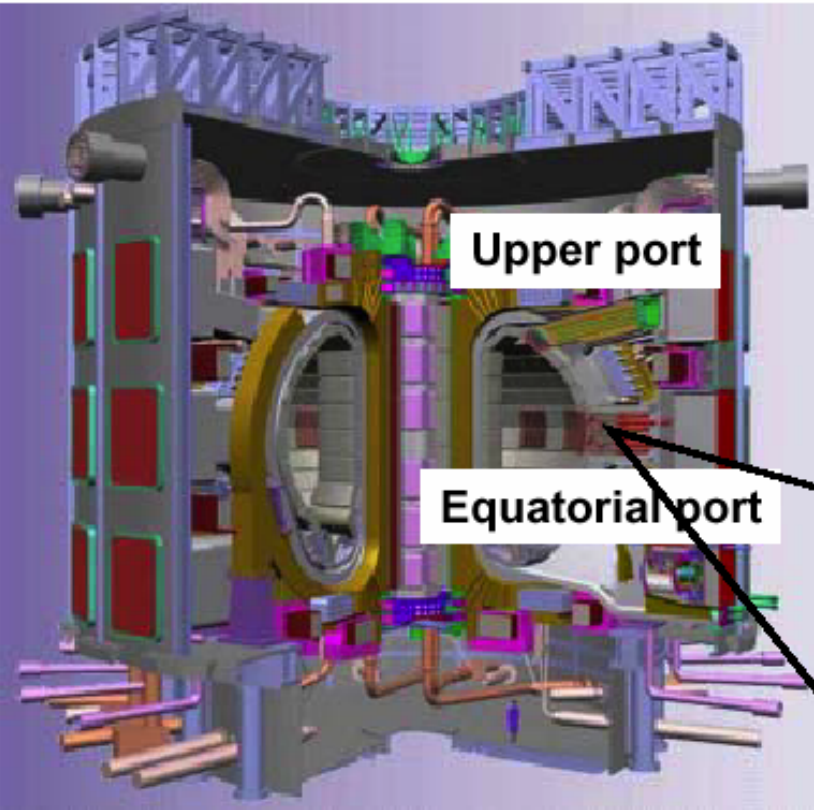
In-vessel mirrors:
thermal loads depending on design

Temperature on radiation-cooled screens:

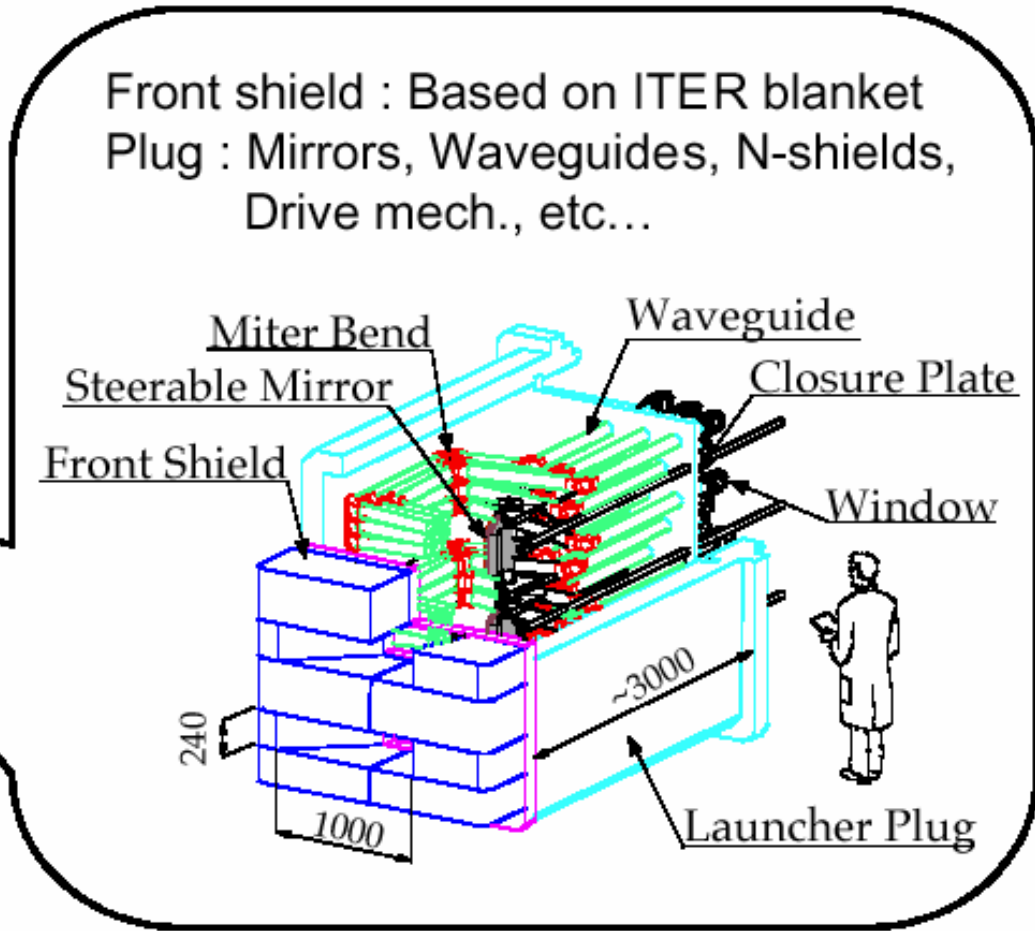


Equatorial EC Launcher

ITER 3D view



Launcher 3D view



Mechanical tests of a flexible cooling tube

JAERI

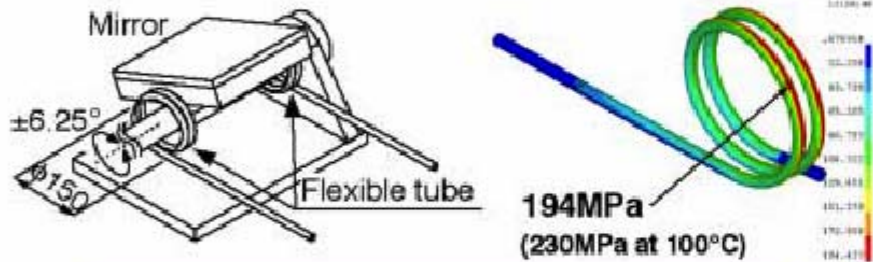
Analysis model

Tube : $\phi_{in/out} = 10/12$, SS316

Rot. θ : $\pm 6.5^\circ$

Internal pressure: 2MPa

Result



Fatigue tests (on-going)

Tube : Same as design

Rot. θ : $\pm 6.5^\circ$

Rot. vel. : 1.3 °/sec

Internal pressure : 2MPa

So far, 2.0×10^4 cycles are succeeded.

- Life time of the tube would be 3×10^4 cycles considering the fatigue data*(cycles to failure at 200MPa loading : $\sim 10^5$) and the safety factor of 1/3.

*A. Baumel Jr. and T. Seeger, "Material Data for Cyclic Loading", 61, Suppl. 1 (1990), Elsevier Science. Co.



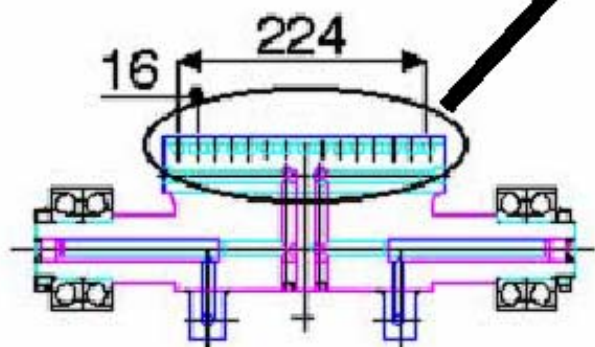
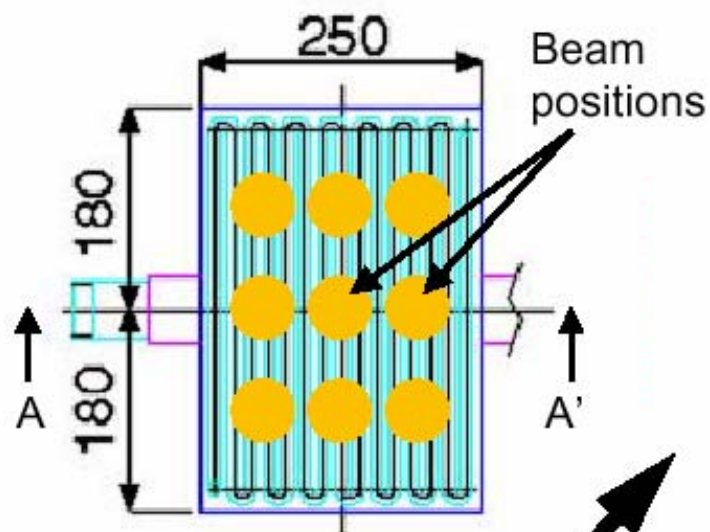
Flexible tube



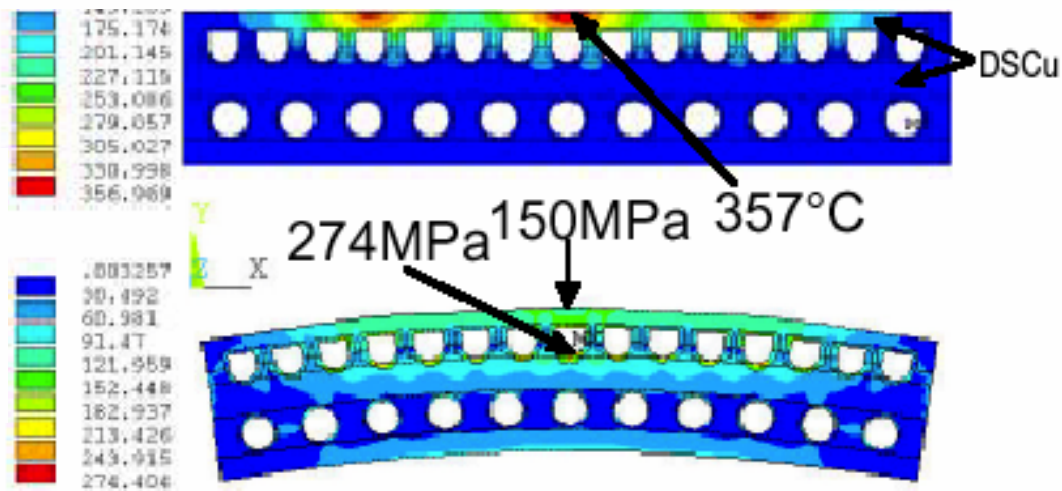
Bearings (WC alloys)

Steering mirror (Design and analysis model)

JAERI



A-A' cross section
Mirror design



Flow velocity : 2m/sec

Calculation condition

Ave. Heat flux: 0.2MW/m^2

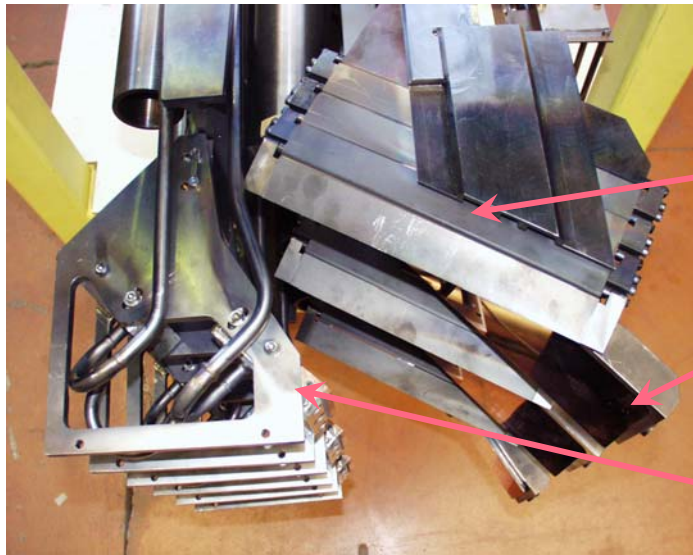
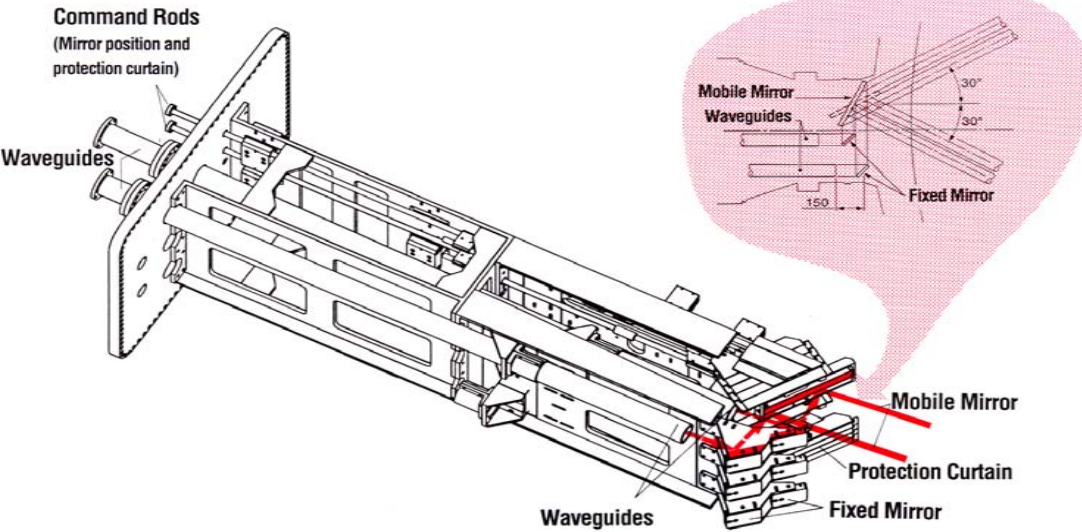
Nuclear heating : 1.0MW/m^3

RF heat load(peak) : 3.1MW/m^2

RF distribution : Gaussian

The Tore Supra Antenna System

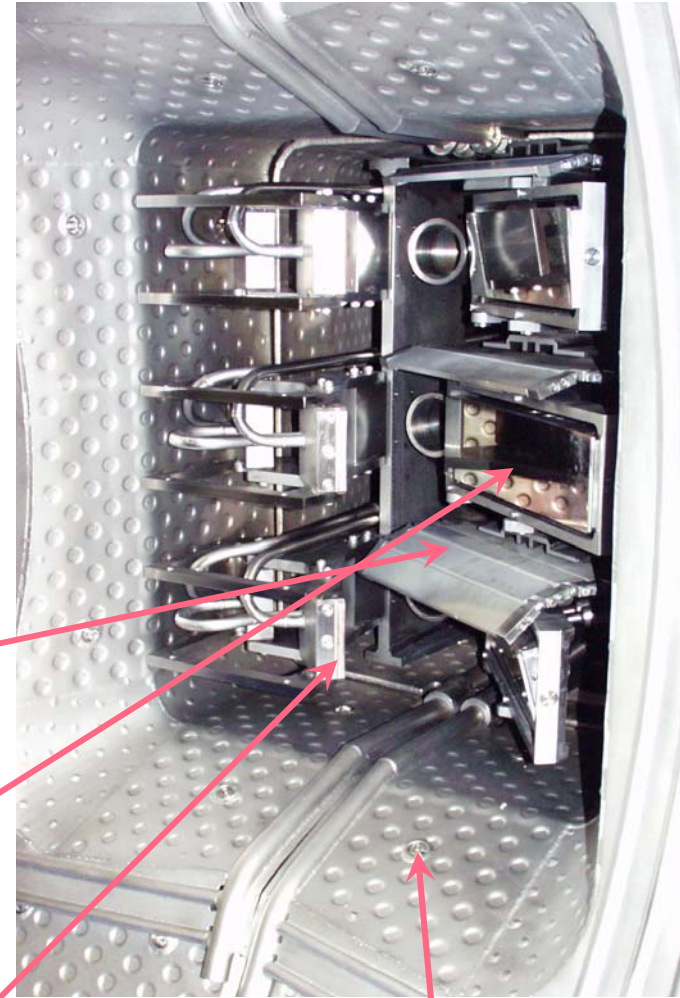
CEA Cadarache



Retractable Protection

3 Mobile Mirror

6 Fixed Mirror



Thermal port protection

Summary

- **CW lines:** **minimization of loss for all components !**
Probably each component needs cooling

- **Launchers:** **high reliability required,**
careful engineering of critical components necessary